



## Outside Air Control – the most cost-effective energy efficiency measure of all

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### Summary

- Problem: most mechanically ventilated buildings supply too much OA (outside air).
- This causes higher heating and cooling loads.
- Remedying this using CO<sub>2</sub> sensing offers very large potential energy savings.
- Estimated value: **\$70 million/year** (in NZ)  
**\$30 billion/year** (world-wide)
- Emissions red'n: **300 kT CO<sub>2e</sub>/yr** (0.4% of NZ total)  
**100 MT CO<sub>2e</sub>/yr** world-wide



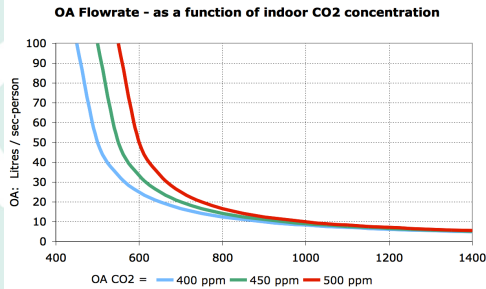
### Why supply fresh air?

- To maintain indoor air quality.
- To allow pressurisation of building interior to avoid infiltration, especially at ground level.  
(This includes replacing exhaust air.)
- To give “free cooling” via “economiser cycle”.




### Ventilation Rates from CO<sub>2</sub> levels

OA Flowrate - as a function of indoor CO<sub>2</sub> concentration




OA CO<sub>2</sub> = 400 ppm 450 ppm 500 ppm



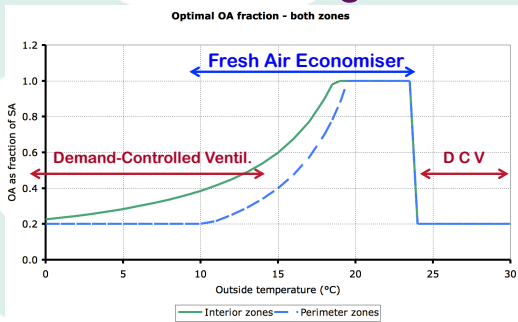

### Definitions

- **ECONOMIZER** – A system of fans, dampers and controls to reduce cooling loads, by increasing OA in certain temperature ranges.
- **DEMAND CONTROLLED VENTILATION** – A system of fans, dampers and controls to reduce heating and cooling loads, by reducing OA.



### OA Control Strategies vs. T

Optimal OA fraction - both zones

### Heating / Cooling Load Calcs

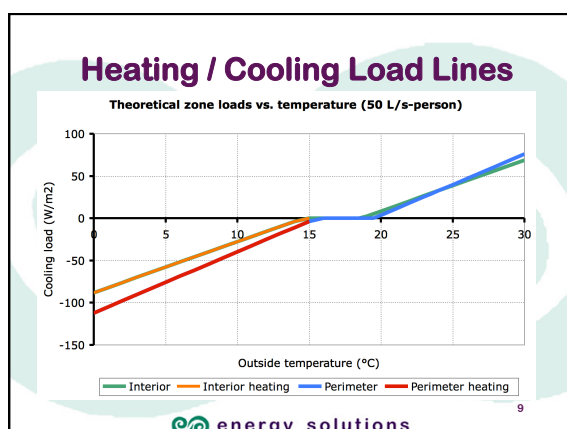
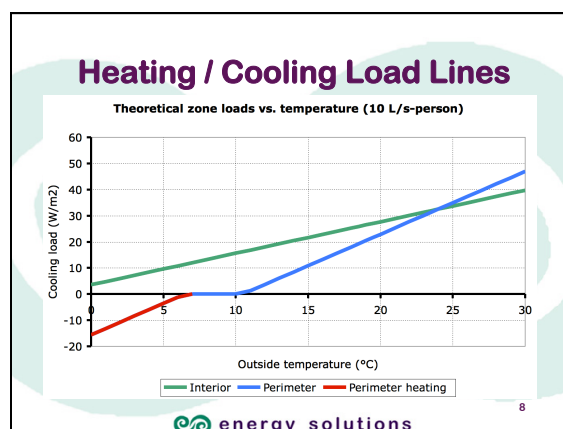
Occupied floors above and below

5 m      10 m      3 m

Walls:  $[A/R] = 20 \text{ m}^2 \div R-2 = 10 \text{ W/}^\circ\text{C}$   
 Windows:  $= 10 \text{ m}^2 \div R-0.33 = 30 \text{ W/}^\circ\text{C}$   
 Ventilation:  $= 5 \text{ people} \times 10 \text{ L/s-p} \times 1.2 = 60 \text{ W/}^\circ\text{C}$   
 Infiltration:  $= 0.4 \text{ AC/h} \times 150 \text{ m}^3 \times 0.33 = 20 \text{ W/}^\circ\text{C}$

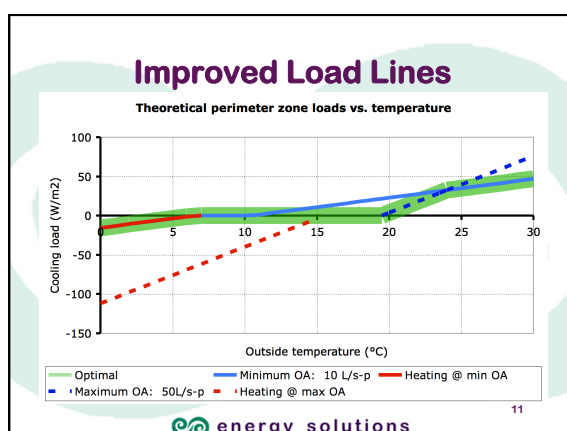
Total heat losses:  $= 120 \text{ W/}^\circ\text{C}$

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If your building is in heating mode...  
 Then the outside air quantity should be at its minimum

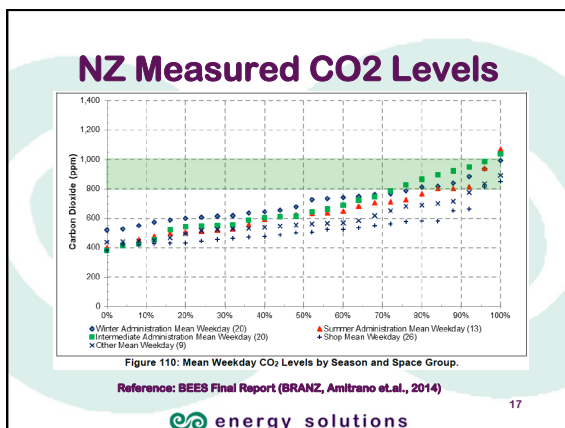
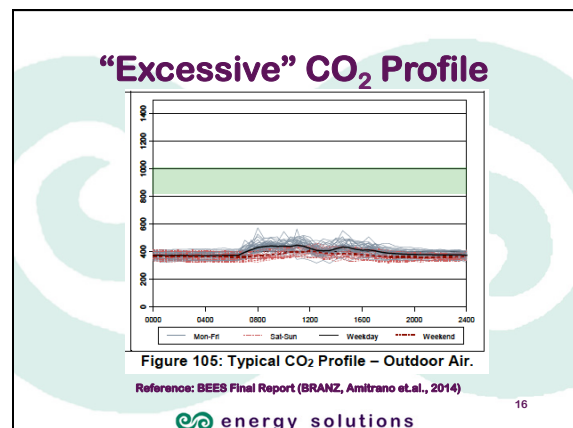
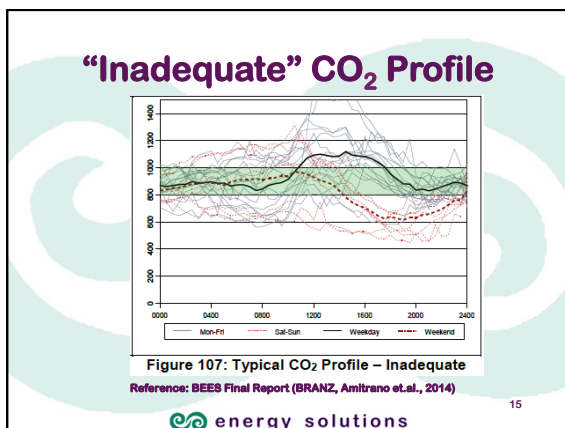
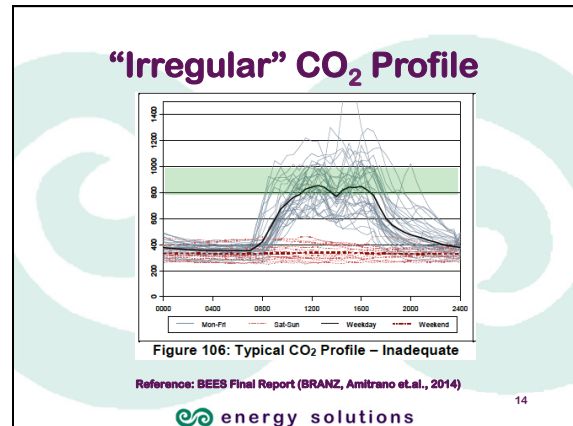
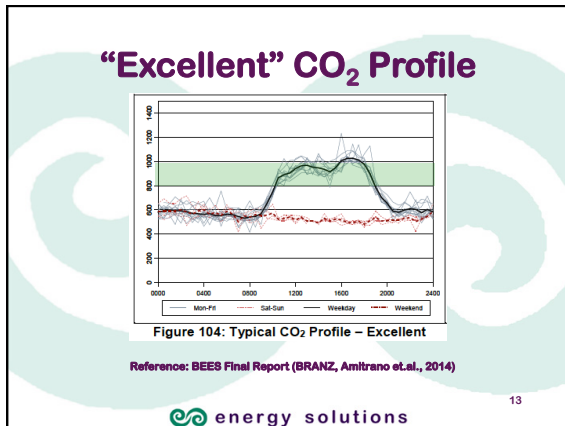
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### What do we know about NZ?

- BEES logged actual CO<sub>2</sub> concentrations in ~100 random NZ “Non-residential” buildings.
- The next graphs show 24-hour load profiles of CO<sub>2</sub>, and the range of results.
- These can be used to infer real OA ventilation rates.

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### U.S. Field Observations

- “... we rarely see interior air CO<sub>2</sub> levels exceed 600 or 800 ppm” (Charles Copeland, ASHRAE Journal, August 2012)
- “... only about one in four economizers works properly” (Liescheidt, Esource, 2000)
- “Economisers show a high rate of failure ... 24% would not move at all” (Jacobs, AEC, 2003)

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### NZ Observed CO<sub>2</sub> levels



This reads 516 ppm.  
This reads 520 ppm.

This is a well-managed large building in mid-winter, supplying about 10x too much outside air.

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### NZ Standard 4303:1990

- Ventilation for Adequate Indoor Air Quality
- Based on ASHRAE 62.1-1989.
- **Ventilation Rate Procedure:** 10 L/sec-person.
- **IAQ Procedure:** Indoor CO<sub>2</sub> concentration under 1100 ppm, or 700 ppm above outdoors, indicates good air quality.

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### ASHRAE Standard 62.1

- Through 2004, Standard only considered ventilation per person. Typically 7 – 10 L/s per person.
- Post 2004 Standards reduces air per person, but adds a term per floor area – effectively the same, but dependent on people density.
- Standard 62.1:2013 typically requires 2.5 L/s-person plus 0.3 L/s – square metre

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### Cooling load calculations

$SA (L/s) = Load (W) / \Delta T_{air} \times 1.21 W/(L/s) \cdot ^\circ C$

So, **SA** quantities for different situations  
(@ 15 W/m<sup>2</sup> electrical loads):

Room type	m <sup>2</sup> /person	L/s-person	L/s-m <sup>2</sup>
Office	10 m <sup>2</sup>	19 L/s-p	1.9 L/s-m <sup>2</sup>
Office	20 m <sup>2</sup>	31 L/s-p	1.5 L/s-m <sup>2</sup>
Stores	100 m <sup>2</sup>	130 L/s-p	1.3 L/s-m <sup>2</sup>
Meeting rm.	2 m <sup>2</sup>	9 L/s-p	4.3 L/s-m <sup>2</sup>

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### Required OA Quantities

Compare the minimum **OA** quantities  
(NZS 4303:1990 vs. ASHRAE 62.1:2013)

Room type	OA L/s-person (NZS / ASHRAE)	RA CO <sub>2</sub> (NZS / ASHRAE)
Office (10 m <sup>2</sup> /p)	10 / 5.5	950 / 1360
Office (20 m <sup>2</sup> /p)	10 / 8.5	950 / 1040
Stores (100 m <sup>2</sup> /p)	10 / 32.5	950 / 600
Meeting (2 m <sup>2</sup> /p)	10 / 3.1	950 / 2100

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### The “Meeting room” problem

Densely and irregularly occupied spaces can have difficult-to-meet ventilation requirements.

Required OA per person can be more than total SA.

Boosting (SA) ventilation to crowded meeting rooms can cause over-cooling if OA need is met.

Solution: either supply dedicated OA duct, or install reheat coils in meeting rooms to prevent over-cooling, and ensure sufficient SA is available.

Otherwise, cooling and vent loads won't be met.

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### Recommendation re. Standards

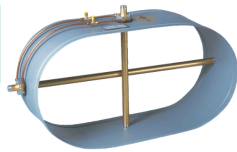
- Supply enough OA to comply with BOTH new ASHRAE and Aus/NZ ventilation standards.
- In NZ, this will only require more ventilation in lightly occupied spaces – storerooms, etc.
- *(But the problem is: most buildings supply much too much OA)*

### Typical control of OA

- Simplest method: If using OA economiser, set minimum position on actuator of moveable OA damper.
- How is it set? Commissioned?
- Is this really “controlling” OA?

### Other OA control methods

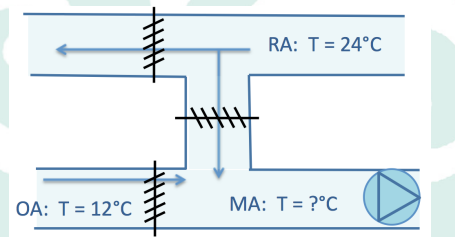
- Separate variable OA damper, or damper and duct. Same problem.
- Or, direct flow measurement station
- Problem: cost.



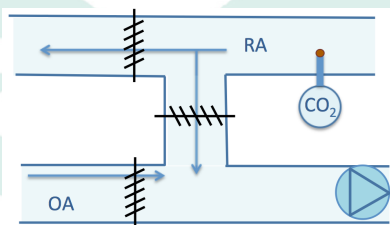
(image from Dwyer Instruments)

### Other OA control methods

- Temperature balance in mixed air.

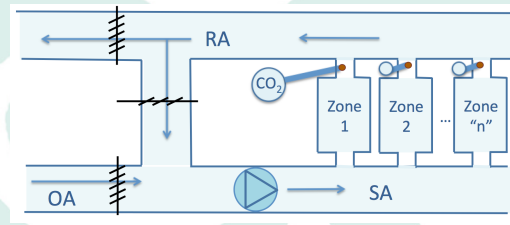


### Typical “DCV” control



- Problem: RA is mixed, zones don't have equal CO2 concentrations

### Improved “DCV” control



- Problem: expense and complication

### Preferred "SADCV" control

• Control dampers based on maintaining SA (or MA) CO<sub>2</sub> level to meet maximum load

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### Calcs for "SADCV" control

- Calculate the design ventilation conditions (SA L/s per zone from loads and occ'y)
- Define the "Target" RA CO<sub>2</sub> concentration (Typically ~1,000 ppm, unless reset)
- Calculate required SA CO<sub>2</sub> to meet design
 
$$[SA\ CO_2] = [RA\ CO_2] - \frac{\# \text{ people} \times CO_2/p}{SA \text{ flowrate L/s}}$$
 (Typically CO<sub>2</sub>/person = 0.005 L/s-person)

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### Basic "SADCV" control

Dampers controlled by SA CO<sub>2</sub> concentration. 900 ppm SA (MA) will meet ventilation design, with 1000 ppm RA target.

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### "SADCV" at part occupancy

Lower RA CO<sub>2</sub> allows OA damper to close more. If any zone is at design capacity, 900 ppm SA (MA) will provide sufficient ventilation.

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### "SADCV" at low occupancy

Still lower RA CO<sub>2</sub> allows OA damper to close even more, to maintain 900 ppm SA. Still meets design ventilation rate for any zone.

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### If Target RA CO<sub>2</sub> is reset...


Same situation holds. Still meets design ventilation rate for any zone.

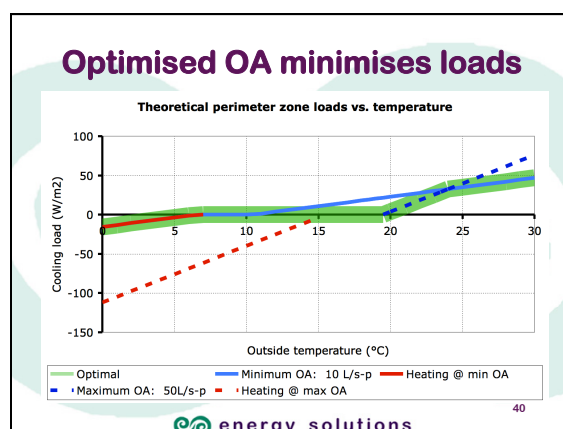
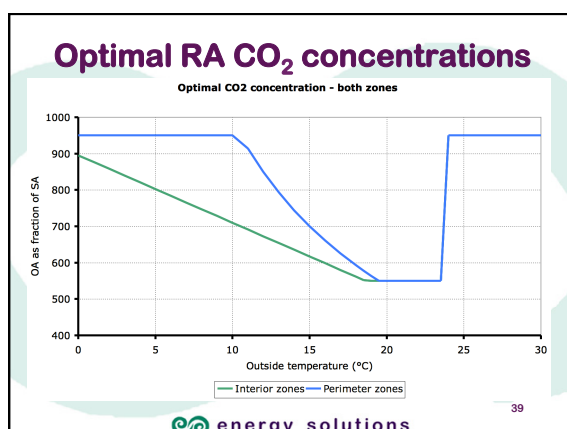
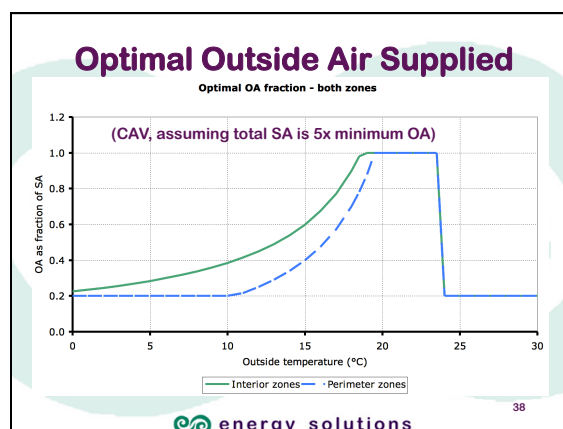
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### Optimisation of OA

- Manage delivery of OA to building (by resetting target SA CO<sub>2</sub>), to minimise heating and cooling loads.
- Effective economiser, between 15 - 22°C.
- Effective DCV, below 15°, above 22°C.
- Significant (up to 90+%) heating and cooling energy savings.
- Potential of avoiding cost and space of boilers in mild climates -> capital cost savings

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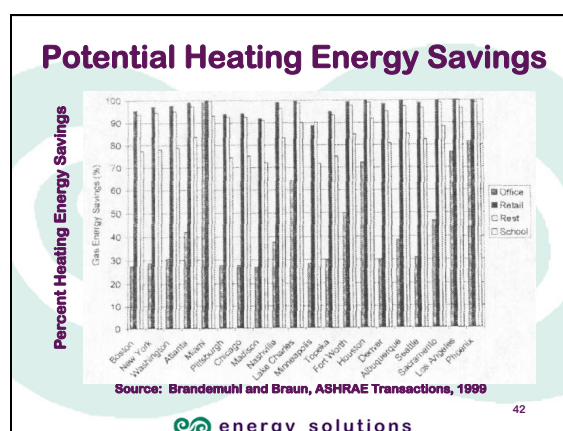


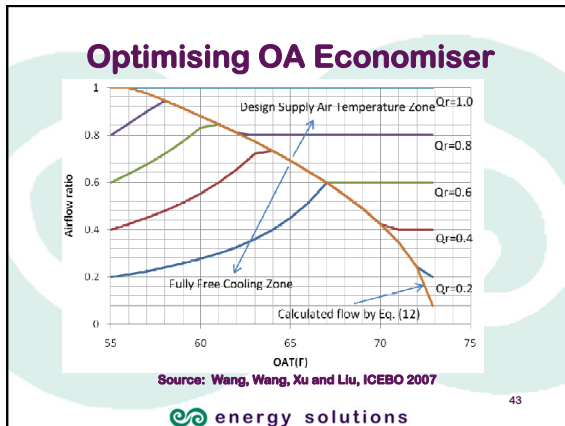
### International research – three separate streams

- Effects of DCV, assuming that buildings were already achieving 1000 ppm.
- Measurements of indoor CO<sub>2</sub>, indicating that buildings generally have very low CO<sub>2</sub>.
- Warnings about the effects of reducing ventilation too much.

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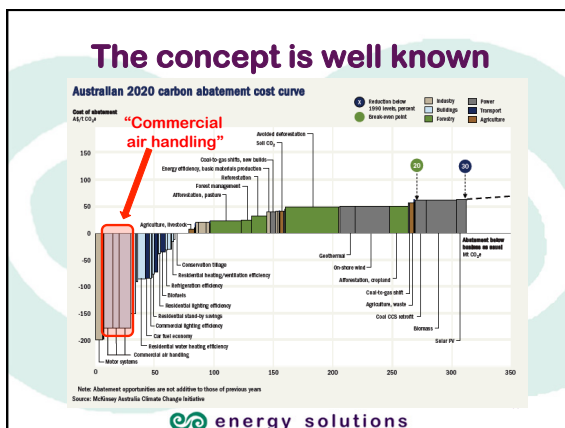
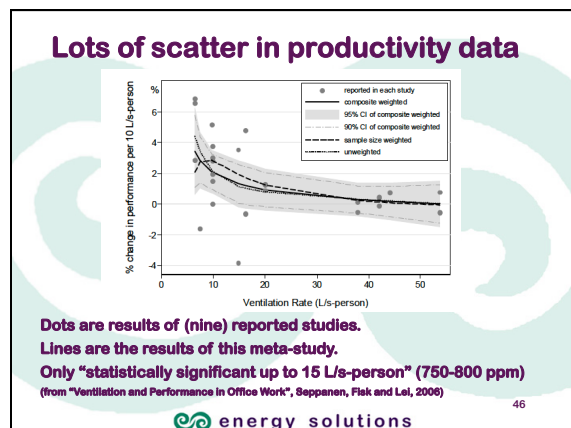
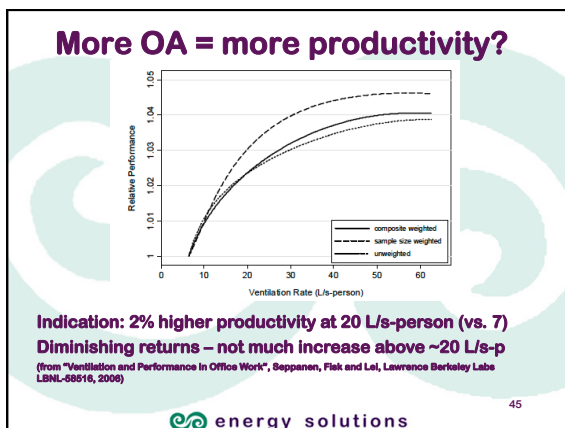




### Concerns with DCV

- Multiple zone systems have intra-zone interactions; CO<sub>2</sub> levels can vary within zones.
- “Acceptable” CO<sub>2</sub> levels can be >3000 ppm.
- CO<sub>2</sub> sensors are very prone to drift.
- Risks of insufficient OA: much higher costs (productivity losses) than potential savings.
- Solution: Use a continuous minimum ventilation rate, with safety factor, recalibrate sensors regularly (daily).**

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### From ASHRAE’s Energy Audits book

First recommendation listed under HVAC systems :

“Reduce HVAC system outdoor airflow rates when possible.”

(from “Procedures for Commercial Building Energy Audits”, ASHRAE 2011, Second edition)

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### Wulfinghoff provides 60 pages

“Measure 4.2.1 Adjust outside air intake...”

Savings potential: May be a large fraction of the cost of heating and cooling energy.

Cost: small, in cases where only adjustments are required.

Payback period: Less than one year.”

(from “Wulfinghoff Energy Efficiency Manual, Energy Institute Press 1999, pp. 516-578)

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### NZ Market - bottom up estimate

- 40% of NZ commercial building floor area is in buildings larger than 3,500 sq.m.
- 500 buildings ~17,000 m<sup>2</sup> (> 9,000 m<sup>2</sup>)  
EnPI<sub>e</sub> = 223 kWh/m<sup>2</sup> yr
- 1,500 buildings ~ 5,200 m<sup>2</sup> (3,500 – 9,000 m<sup>2</sup>)  
EnPI<sub>e</sub> = 201 kWh/m<sup>2</sup> yr
- 3,500 buildings ~ 2,200 m<sup>2</sup> (1,500 – 3,500 m<sup>2</sup>)  
EnPI<sub>e</sub> = 155 kWh/m<sup>2</sup> yr

Data from BEES Final Report (BRANZ, Amtrano et al., 2014)

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### NZ HVAC EnPIs by building size

Reference: BEES Final Report (BRANZ, Amtrano et al., 2014)

Figure 64: EnPI<sub>elec</sub> of Premises by Building Size Strata.

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### NZ HVAC EnPIs by building use

Reference: BEES Final Report (BRANZ, Amtrano et al., 2014)

Figure 62: EnPI<sub>elec</sub> of Premises by Building Use Strata.

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### NZ HVAC System types

Strata	Fixed Gas	Portable Gas	Portable Electric	Fixed Resistance	Heat Pump	Central HVAC
S1	4%	2%	26%	10%	62%	0%
S2	4%	26%	4%	0%	57%	1%
S3	0%	0%	20%	8%	60%	1%
S4	0%	0%	0%	23%	54%	23%
S5	0%	0%	0%	0%	1%	88%

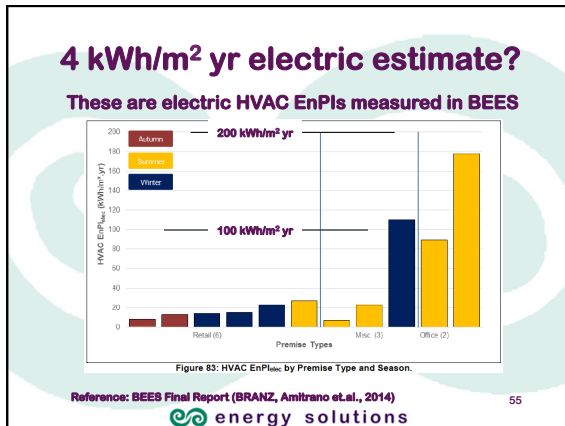
Reference: BEES Final Report (BRANZ, Amtrano et al., 2014)

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### NZ Market - bottom up estimate

- Top 500 buildings > 9,000 m<sup>2</sup>. Avg. 17,000 m<sup>2</sup>  
EnPI<sub>e</sub> = 223 kWh/m<sup>2</sup> yr; EnPI gas ~100 kWh/m<sup>2</sup> yr
- ~20% cooling red'n = 4 kWh/m<sup>2</sup> yr electric; 27 GWh/yr
- ~50% heating red'n = 50 kWh/m<sup>2</sup> yr gas; 300 GWh/yr
- Value = \$40k/yr per building = \$20M/yr
- CO<sub>2e</sub> reduction 160 T/yr per building = 80 kT/yr

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- ### NZ Market - top down estimate
- Commercial sector electricity = 9,500 GWh/y;
  - Com'l gas = 2,000 GWh/y (Energy Data File 2012)
  - Electric energy reduction: 50% Buildings x 33% HVAC x 50% cooling x 20% reduction = **160 GWh/yr** (4 kWh/m<sup>2</sup> yr)
  - Gas energy reduction: 80% buildings x 90% HVAC x 70% reduction = **1,000 GWh/yr** (25 kWh/m<sup>2</sup> yr)
  - Value = **\$70 M/yr** (@ 15¢/kWh<sub>e</sub>, 5¢/kWh<sub>g</sub>)
  - CO<sub>2e</sub> reduction **300 kT/yr** (0.4% of NZ total)
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- ### World Target Market
- Most major countries have similar energy consumption distributions to New Zealand.
  - Australia = NZ potential x 6
    - Potential savings = **\$400 M/yr**, **2 MT CO<sub>2e</sub>/yr**
  - USA = NZ potential x 100
    - Potential savings = **\$7 B/yr**, **30 MT CO<sub>2e</sub>/yr**
  - World = NZ potential x 500
    - Potential savings = **\$30 B/yr**, **100 MT CO<sub>2e</sub>/yr**
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- ### Summary
- CO<sub>2</sub> sensing allows control of OA.
  - SA CO<sub>2</sub> is preferred control point.
  - Up to 90% heating energy savings, ~20% cooling energy savings result.
  - NZ Value: **\$20M - \$70M/yr.**
  - NZ emissions red'n: **80 kT – 300 kT/yr.**
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- ### Do it right.
- Control OA delivery to spaces by measuring CO<sub>2</sub> concentration in **SUPPLY AIR.**
  - Re-calibrate CO<sub>2</sub> sensors **DAILY** using full OA, automatically.
  - Keep records (trend logs) to prove you haven't compromised comfort.
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